

MHD flow of hybrid nanofluid past a stretching sheet: double stratification and multiple slips effects

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Studies of hybrid nanofluids flowing over various physical geometries and conditions are popular among researchers to understand the behavior of these fluids. Thenceforth, the numerical solutions for hybrid Ag-CuO/H₂O nanofluid flow over a stretching sheet with suction, magnetic field, double stratification, and multiple slips effects are analyzed in the present study. Governing equations and boundary conditions are introduced to describe the flow problem. Then, similarity variables are applied to transform the equations into non-linear ordinary differential equations and boundary conditions. The numerical computation for the problem is done in Matlab (bvp4c solver), and the results are presented in tables and graphs. It is found that the rise in solutal slip and stratification parameters reduces the Sherwood number. Meanwhile, the increase in thermal slip and stratification parameters lowers the Nusselt number. The skin friction coefficient is observed to increase with the augmentation of the hydrodynamic slip parameter.

Keywords: *hybrid nanofluid, double stratification, slips, MHD, stretching sheet.*

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1. Introduction

The suspension of two or more different nanoparticles with a size of less than 100 nm in a base fluid produces a new generation of nanofluid, known as hybrid nanofluid [1]. The usual combination of nanoparticles is from carbon nanotubes, oxide nanoparticles, and metallic nanoparticles dispersed in a base fluid, usually water (H₂O), organic fluids, engine oils, and polymeric solutions. Hybrid nanofluids have similar applications to nanofluids in all fields of heat transfer, such as in biomedical, air-conditioning systems, heat exchangers, coolant in machining and manufacturing, solar energy, and transportation [1, 2]. However, the mixture of dissimilar nanoparticles with different characteristics makes hybrid nanofluids more superior to nanofluids and other conventional heat transfer fluids in terms of higher thermal conductivity and better thermophysical properties. Fluid flow over a stretching sheet is significant in various industrial and manufacturing processes. For example, fluid processing units operated on roller belts, paper industry and extrusion process, drawing of copper wires, manufacturing of aluminum bottle process, and production of rubber and plastic sheets [3, 4]. Devi and Devi [5] studied the flow of hybrid nanofluid over a stretching sheet with suction and magnetic field. In this study, Cu-Al₂O₃/H₂O hybrid nanofluid was found to have a higher heat transfer rate than the Cu/H₂O nanofluid. The greater efficiency of hybrid nanofluid compared to nanofluid was also agreed upon by Prakash and Devi [6] and Hayat and Nadeem [2] in studies involving different flow conditions

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of various hybrid nanofluids over a stretching sheet. Dinarvand et al. [7] investigated the usage of hybrid nanofluid in the biomedical field by simulating a drug delivery system using CuO-Cu/blood hybrid nanofluid flow over a porous stretching sheet in the presence of a magnetic field. It was found that the magnetic field reduces the blood velocity, and blade-shaped nanoparticles provide the best heat transfer performance in the flow. Meanwhile, Aly and Pop [8] reported that the Cu-Al₂O₃/H₂O hybrid nanofluid works as a good heater on increasing magnetic field but turns as a better cooler on increasing Eckert number, stretching, and slip parameters. Jusoh et al. [9] found that the presence of convective boundary condition in the flow of hybrid nanofluid enhances the heat transfer rate, and the usage of kerosene as the base fluid is better than water and methanol. Wahid et al. [10] exposed that velocity slip reduces the velocity profile of Cu-Al₂O₃/H₂O hybrid nanofluid, but the existence of thermal radiation boosts the temperature profile of the fluid. The three-dimensional rotating flow of Ag-Al₂O₃/H₂O hybrid nanofluid past a stretching sheet was discussed by Shoaib et al. [11]. Whereas the unsteady flow of hybrid nanofluid over a stretching sheet was analyzed by Sreedevi et al. [12] and Santhi et al. [13]. In addition, there are also other recent studies related to hybrid nanofluid flow over a stretching sheet (see [14–22]).

Stratification and slips can occur in the flow of a heterogeneous fluid. The layering of the fluid system due to the temperature, concentration, or density differences is called stratification. For example, stratification of heterogeneous mixtures in industrial, food, and manufacturing processes [23]. Meanwhile, the inclusion of slip boundary condition in the flow of foams, suspensions, emulsions, and polymer solutions is familiar in real-life applications (e.g., melting of polymers, in drug delivery systems, microelectronic cooling systems, and micro heat exchangers) [24–26]. Rozeli et al. [27] analyzed the effects of double stratification and slips on the MHD stagnation point flow of a viscous fluid over a stretching/shrinking sheet in a porous medium. Whereas, the effects of suction and double stratification on micropolar fluid flow over a shrinking sheet were analyzed by Khashi'ie et al. [28]. Meanwhile, Hayat et al. [24] studied the effects of these parameters on the MHD flow of nanofluid over a stretching cylinder. The current study will extend these studies to the case of hybrid nanofluid, suiting the recent interest in the field of fluid dynamics. In the present study, the magnetohydrodynamics (MHD) flow of Ag-CuO/H₂O hybrid nanofluid, past a stretching sheet embedded in a porous medium, will be discussed. The mathematical formulation of the flow problem, consisting of the governing partial differential equations and boundary conditions, will be established along with the effects of slips, stratification, Brownian motion, thermophoresis, and nanoparticle volume fraction. Then, suitable similarity variables will be employed to transform the equations and boundary conditions into non-linear ordinary differential equations before being solved numerically in Matlab using the bvp4c solver. The results in this study are original and will provide a significant contribution to the study of hybrid nanofluid in fluid dynamics and other related fields.

2. Problem geometry with mathematical formulation

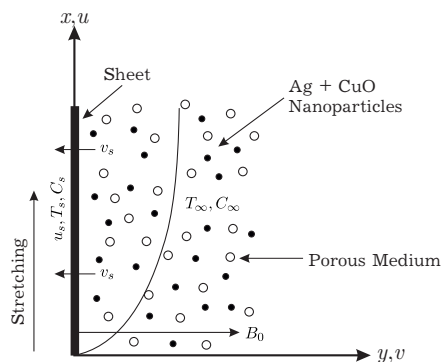


Fig. 1. Geometry of the problem and coordinate system.

The geometry of the flow problem is represented by the Cartesian coordinates of x and y -axes. The velocities along these axes are given by u and v , respectively. As illustrated in Fig. 1, the working fluid, Ag-CuO/H₂O hybrid nanofluid, is assumed to flow over a sheet with a stretching velocity of $u_s = ax/L$, a mass transfer velocity of $v_s < 0$ for suction, and is embedded in a porous medium with a permeability of K_p . The temperature and concentration at the sheet surface are $T_s = T_0 + bx/L$ and $C_s = C_0 + dx/L$, respectively. Whereas the temperature and concentration of the free stream hybrid nanofluid are stratified at $T_\infty = T_0 + cx/L$ and $C_\infty = C_0 + ex/L$, re-

spectively. Here, $a, b, c, d,$ and e are constants. Meanwhile, an additional effect magnetic field with strength B_0 is imposed in the perpendicular direction of the sheet, and the induced magnetic field is neglected due to the low magnetic Reynolds number. Brownian motion and thermophoresis are considered, with a Brownian diffusion coefficient, D_B and thermophoretic diffusion coefficient, D_T .

For the mathematical formulation, the nanofluid models by Buongiorno [29] and Tiwari and Das [30] are implemented to study the effects of Brownian motion, thermophoresis, and nanoparticle volume fraction on the hybrid nanofluid flow. The governing equations for the stated steady, two-dimensional flow problem are [24, 27, 31, 32]:

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} = 0, \tag{1}$$

$$u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} = \frac{1}{\rho_{hn}} \left[\mu_{hn} \frac{\partial^2 u}{\partial y^2} - \frac{\mu_{hn}}{K_p} u - \sigma_{hn} B_0^2 u \right], \tag{2}$$

$$u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} = \frac{1}{(\rho C_p)_{hn}} \left[k_{hn} \frac{\partial^2 T}{\partial y^2} + \frac{[(\rho C_p)_{hn}]^2}{(\rho C_p)_{bf}} \left(D_B \frac{\partial C}{\partial y} \frac{\partial T}{\partial y} + \left(\frac{D_T}{T_\infty} \right) \left(\frac{\partial T}{\partial y} \right)^2 \right) \right], \tag{3}$$

$$u \frac{\partial C}{\partial x} + v \frac{\partial C}{\partial y} = D_B \frac{\partial^2 C}{\partial y^2} + \left(\frac{D_T}{T_\infty} \right) \frac{\partial^2 T}{\partial y^2}, \tag{4}$$

which consist of the continuity equation (1), momentum equation (2), energy equation (3) and concentration equation (4). In the governing equations, ρ, μ, σ, k and ρC_p represent the density, dynamic viscosity, electrical conductivity, thermal conductivity, and heat capacity of the fluid, respectively. Meanwhile, the suffixes of $hf, bf, nf, n1$ and $n2$ are assigned for hybrid nanofluid, base fluid, CuO nanoparticles and Ag nanoparticles, respectively. The thermophysical properties of the base fluid, nanoparticles, and hybrid nanofluid are described by Devi and Devi [5] and Hayat et al. [33].

Next, the flow problem has the following boundary conditions [31]:

$$u = \lambda u_s + S_1 \nu_{hn} \frac{\partial u}{\partial y}, \quad v = v_s, \quad T = T_s + S_2 \frac{\partial T}{\partial y}, \quad C = C_s + S_3 \frac{\partial C}{\partial y} \quad \text{at } y = 0, \tag{5}$$

$$u \rightarrow 0, \quad T \rightarrow T_\infty, \quad C \rightarrow C_\infty \quad \text{as } y \rightarrow \infty, \tag{6}$$

with ν as the kinematic viscosity, $S_1, S_2,$ and S_3 are the velocity, thermal and solutal slip factors, respectively.

Local Nusselt number, $Nu_x,$ local Sherwood number, $Sh_x,$ and local skin friction coefficient, C_{fx} are the physical quantities of interest that correspond to the heat transfer rates, mass transfer rates, and wall shear stress, respectively. The dimensionless forms of these quantities are

$$Nu_x Da_x^{\frac{1}{2}} = -\frac{k_{hn}}{k_{bf}} \theta'(0), \quad Sh_x Da_x^{\frac{1}{2}} = -\phi'(0), \quad C_{fx} Re_x Da_x^{\frac{1}{2}} = 2 \frac{\mu_{hn}}{\mu_{bf}} f''(0), \tag{7}$$

where $Da_x = K_p/x^2$ and $Re_x = x u_s/\nu_{bf}$ are the local Darcy number and Reynolds number, respectively.

3. Method of solving

Numerical computation will be carried out in Matlab using a finite-difference code-containing solver called the `bvp4c`, which implements the collocation formula known as the three-stage Lobatto IIIa formula [34]. The solver has a syntax of `sol = bvp4c(odefun,bcfun,solinit,options)` that integrates a system of differential equations defined in `odefun` subject to the boundary conditions specified in `bcfun` with the initial guess of solution made in `solinit` and integration settings in `options`.

For the `bvp4c` solver, the differential equations have to be rewritten as first-order differential equations. First, the partial differential equations and boundary conditions (1)–(6) are transformed into a

system of ordinary differential equations by using the similarity variables introduced by Mabood and Usman [31] and Reddy and Sreedevi [35]. Then, the following non-linear ordinary differential equations and boundary conditions are obtained:

$$f''' - f' + (1 - \varphi_{n1})^{2.5}(1 - \varphi_{n2})^{2.5} \text{Re Da} \left[\left(\varphi_{n2} \frac{\rho_{n2}}{\rho_{bf}} + (1 - \varphi_{n2}) \left((1 - \varphi_{n1}) + \varphi_{n1} \frac{\rho_{n1}}{\rho_{bf}} \right) \right) (ff'' - f'^2) - \frac{\sigma_{hn}}{\sigma_{bf}} M f' \right] = 0, \quad (8)$$

$$\theta'' + \left[\varphi_{n2} \frac{(\rho C_p)_{n2}}{(\rho C_p)_{bf}} + (1 - \varphi_{n2}) \left((1 - \varphi_{n1}) + \varphi_{n1} \frac{(\rho C_p)_{n1}}{(\rho C_p)_{bf}} \right) \right] \frac{k_{bf}}{k_{hn}} \text{Pr} [\text{Re Da} (f\theta' - f'\theta - \xi_1 f')] + Nt(\theta')^2 + Nb\phi'\theta' = 0, \quad (9)$$

$$\phi'' + \frac{Nt}{Nb} \theta'' - \text{Re Da Le} (f'\phi + \xi_2 f' - f\phi') = 0, \quad (10)$$

$$f(0) = S, \quad f'(0) = \lambda + S_1^* f''(0), \quad \theta(0) = 1 - \xi_1 + S_2^* \theta'(0), \quad \phi(0) = 1 - \xi_2 + S_3^* \phi'(0), \quad (11)$$

$$f'(\infty) \rightarrow 0, \quad \theta(\infty) \rightarrow 0, \quad \phi(\infty) \rightarrow 0.$$

In the equations, f , θ , and ϕ are functions related to velocity, temperature and nanoparticle concentration profiles, respectively, with $'$ indicates differentiation with respect to η . Meanwhile, the dimensionless parameter φ is the volume fractions of individual nanoparticles, $\text{Re} = (aL)/\nu_{bf}$ is the Reynolds number, $\text{Da} = K_p/L^2$ is the Darcy number, $M = (\sigma_{bf} B_0^2 L)/(a\rho_{bf})$ is the magnetic field parameter, $\text{Pr} = [\mu_{bf}(\rho C_p)_{bf}]/(\rho_{bf} k_{bf})$ is the Prandtl number, $\text{Nb} = \left[\left(\frac{(\rho C_p)_{hn}}{(\rho C_p)_{bf}} \right) D_B (C_s - C_\infty) \right] / \nu_{bf}$ is the Brownian motion parameter, $\text{Nt} = \left[\left(\frac{(\rho C_p)_{hn}}{(\rho C_p)_{bf}} \right) D_T (T_s - T_\infty) \right] / (\nu_{bf} T_\infty)$ is the thermophoresis parameter, $\text{Le} = \nu_{bf}/D_B$ is the Lewis number, $\xi_1 = c/b$ is the thermal stratification parameter, $\xi_2 = e/d$ is the solutal stratification parameter, $S = -(v_s L)/(a\sqrt{K_p})$ is the suction parameter ($S > 0$), λ is the stretching parameter, $S_1^* = (S_1 \nu_{bf})/\sqrt{K_p}$ is the hydrodynamic slip parameter, $S_2^* = S_2/\sqrt{K_p}$ is the thermal slip parameter, and $S_3^* = S_3/\sqrt{K_p}$ is the solutal slip parameter.

Next, the following substitutions are introduced and substituted into (8)–(11):

$$f = y(1), \quad f' = y(1)' = y(2), \quad f'' = y(2)' = y(3), \quad f''' = y(3)',$$

$$\theta = y(4), \quad \theta' = y(4)' = y(5), \quad \theta'' = y(5)',$$

$$\phi = y(6), \quad \phi' = y(6)' = y(7), \quad \phi'' = y(7)'.$$

The resulting first-order ordinary differential equations and boundary conditions are then coded into the `odefun` and `bcfun` of the `bvp4c` solver, respectively. A detailed explanation and examples are shown in the study by Yahaya et al. [36]. The numerical results are recorded, analyzed, and discussed.

4. Results and discussion

The plots of velocity ($f'(\eta)$), temperature ($\theta(\eta)$), and concentration ($\phi(\eta)$) against η with various pertinent parameters are presented in this section. According to Pantokratoras [37], the gradients for velocity, temperature and concentration profiles at some distance away from the sheet should be zero after achieving the free stream condition (as $\eta \rightarrow \infty$) of the boundary layer flow. In this study, all profiles reach the free stream condition, stated in (11), correctly (asymptotically), which verifies the correctness of the profiles and numerical results. Besides that, the numerical results computed using the `bvp4c` solver are in a good agreement with the previous results by Mabood and Usman [31] that are computed using the homotopy analysis method (HAM), as shown in Table 1. However, the

temperature profiles obtained in this study show an undershoot of temperature or negative temperature. The observed behavior may be due to the high magnitude of the thermal stratification parameter used in this study. The same behavior was also reported by Srinivasacharya and Surender [38], Sarojamma et al. [39], and Khashi'ie et al. [40].

The effects of nanoparticle volume fraction of Ag, φ_{n2} on velocity profile are depicted in Fig. 2a. The increase in φ_{n2} is found to reduce the velocity profile of the hybrid nanofluid. The momentum boundary layer thickness reduces, and the skin friction coefficient decreases with the addition of φ_{n2} . Meanwhile, the temperature profile in Fig. 2b shows an improvement with the increasing value of φ_{n2} . Khashi'ie et al. [41] stated that nanoparticles dissipate heat energy. Thus, adding more nanoparticles will raise the temperature of the hybrid nanofluid and causes the temperature profile to increase. Since Ag nanoparticles have high thermal conductivity, the introduction of more of these nanoparticles into the hybrid nanofluid enhances the Nusselt number $\left[= -\frac{k_{hn}}{k_{bf}}\theta'(0) \right]$, as shown in Table 2. Thus, incorporating a certain amount of metallic nanoparticle Ag into the hybrid nanofluid can improve the heat transfer performance of the fluid. However, as shown in Fig. 2b, the increase in φ_{n2} lowers the concentration profile of the hybrid nanofluid near the sheet. After some distance from the sheet, the concentration profile improves with φ_{n2} .

Table 1. Comparison of $-f''(0)$ at $Pr = 6.8, Re = 5, \lambda = 1, Le = 5, Da = M = S = \varphi_{n1} = \varphi_{n2} = \xi_1 = \xi_2 = 0,$ and $Nb = Nt = 0.1.$

| S_1^* | S_2^* | S_3^* | $-f''(0)$ | |
|---------|---------|---------|---------------|-----------------------|
| | | | Present study | Mabood and Usman [31] |
| 1 | 0 | 0 | 0.50000 | 0.50000 |
| 0.4 | 0.5 | | 0.71429 | 0.71429 |
| 0.5 | | 1 | 0.66667 | 0.66667 |

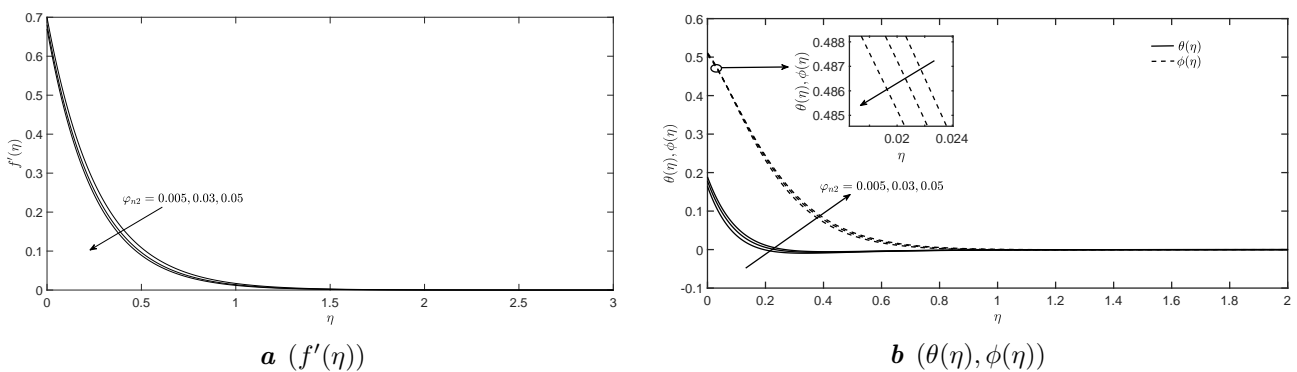


Fig. 2. Velocity, temperature and concentration profiles with varying values of nanoparticle volume fraction of Ag, φ_{n2} .

Next, Fig. 3a illustrates the effects of the hydrodynamic slip parameter, S_1^* on the velocity profile. It is observed that the increase in S_1^* diminishes the velocity profile of the hybrid nanofluid. Physically, hydrodynamic slip causes the fluid velocity near the sheet to be unequal to the stretching sheet. The higher the value of S_1^* , the lower the velocity of the stretching sheet transferred to the hybrid nanofluid. Besides that, the increase in S_1^* produces friction force that enables more fluid to slip past the stretching sheet, which lowers the hybrid nanofluid velocity and raises the temperature. As shown in Fig. 3b, the temperature and concentration profiles increase with S_1^* . The thickness of thermal and concentration boundary layers elevates and reduces the values of $-\theta'(0)$ and $-\phi'(0)$. The Nusselt number and Sherwood number decrease with the rise of S_1^* , as tabulated in Table 2. Contrary, the augmentation of the thermal slip parameter, S_2^* reduces the temperature and concentration profiles displayed in Fig. 4. The decreasing value of the Nusselt number obtained in Table 2 indicates that the rise in S_2^* inhibits the heat transfer performance of the fluid. Less heat is transferred from the hot stretching sheet to the surrounding hybrid nanofluid, which causes the reduction of fluid temperature. Similarly, the increase in solutal slip parameter, S_3^* reduces the concentration profile in Fig. 5 and lowers the mass transfer performance of the hybrid nanofluid, as obtained in Table 2.

Table 2. Values of $C_{fx}Re_xDa_x^{\frac{1}{2}}$, $Nu_xDa_x^{\frac{1}{2}}$ and $Sh_xDa_x^{\frac{1}{2}}$ when $\varphi_{n1} = 0.1$, $Da = 0.5$, $Le = 2$, $Pr = 6.2$, $\lambda = 1.48$, $M = 0.1$ and $Re = 5$.

| φ_{n2} | S | S_1^* | S_2^* | S_3^* | ξ_1 | ξ_2 | Nt | Nb | $C_{fx}Re_xDa_x^{\frac{1}{2}}$ | $Nu_xDa_x^{\frac{1}{2}}$ | $Sh_xDa_x^{\frac{1}{2}}$ |
|----------------|------|---------|---------|---------|---------|---------|------|-----|--------------------------------|--------------------------|--------------------------|
| 0.005 | 0.95 | 0.3 | 0.3 | 0.3 | 0.2 | 0.2 | 0.1 | 0.1 | -6.85857 | 2.84746 | 0.96323 |
| 0.03 | | 0.27 | | | | | | | -7.92900 | 3.00621 | 0.97851 |
| | | 0.3 | 0.4 | | | | | | -7.47832 | 2.40401 | 1.11739 |
| | | | 0.5 | | | | | | -7.47832 | 2.00515 | 1.21638 |
| | | | 0.3 | 0.4 | | | | | -7.47832 | 3.00162 | 0.80274 |
| | | | | 0.5 | | | | | -7.47832 | 3.00374 | 0.68472 |
| | | | | 0.3 | 0.1 | | | | -7.47832 | 3.29969 | 0.89670 |
| | | | | | 0.2 | 0.1 | | | -7.47832 | 2.99507 | 1.14797 |
| | | | | | | 0.2 | | | -7.47832 | 2.99861 | 0.96991 |
| | | | | | 0.3 | | | | -7.47832 | 2.69641 | 1.04343 |
| | | | | | 0.2 | 0.3 | | | -7.47832 | 3.00213 | 0.79185 |
| | | | | | | 0.2 | 0.13 | | -7.47832 | 2.98892 | 0.74926 |
| | | | | | | | 0.15 | | -7.47832 | 2.98240 | 0.60312 |
| | | | | | | | 0.1 | 0.2 | -7.47832 | 2.96746 | 1.34824 |
| | | | | | | | | 0.3 | -7.47832 | 2.93504 | 1.47447 |
| | | 0.31 | | | | | | 0.1 | -7.33966 | 2.99622 | 0.96721 |
| | 0.96 | 0.3 | | | | | | | -7.50009 | 3.00354 | 0.97570 |
| | 0.94 | | | | | | | | -7.45648 | 2.99364 | 0.96411 |
| 0.05 | 0.95 | | | | | | | | -7.99000 | 3.12168 | 0.97705 |

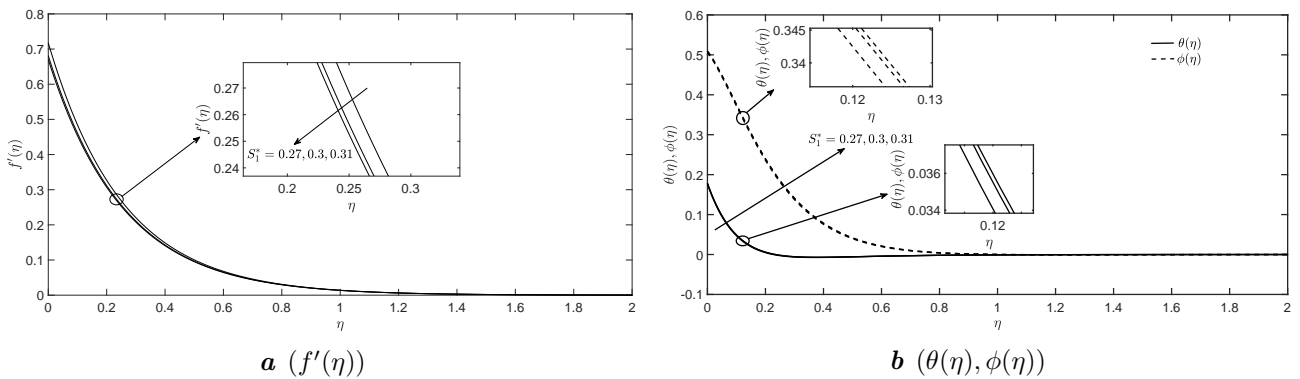


Fig. 3. Velocity, temperature and concentration profiles with varying values of hydrodynamic slip parameter, S_1^* .

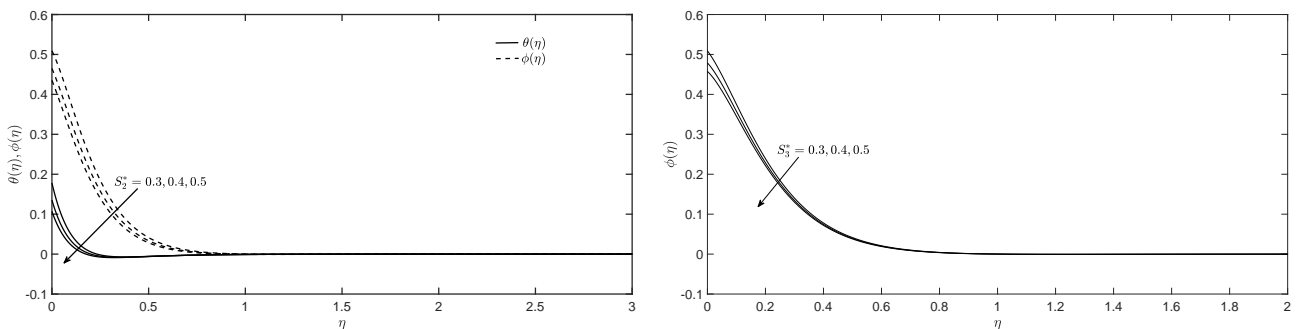


Fig. 4. Temperature and concentration profiles with varying values of thermal slip parameter, S_2^* .

Fig. 5. Concentration profile with varying values of solutal slip parameter, S_3^* .

In Fig. 6, the temperature and concentration profiles are observed to decrease as ξ_1 increases. Similar behavior is observed in Fig. 7 for the increasing value of ξ_2 . However, the enhancement of ξ_1 and ξ_2 affects the Nusselt number and Sherwood number differently, as seen in Table 2. The increase in thermal stratification parameter [$\xi_1 = c/b$] signifies the augmentation of ambient temperature or re-

duction of the surface temperature. Hence, the difference between ambient and surface temperatures diminishes as ξ_1 increases. As a result, the temperature gradient decreases, reducing the heat transfer rate and temperature profile of the hybrid nanofluid. The reduced concentration boundary layer thickness raises the concentration gradient and enhances the Sherwood number. Meanwhile, the Sherwood number drops when ξ_2 increases. The rise in solutal stratification parameter [$\xi_2 = e/d$] describes the enhancement of ambient fluid concentration or depletion in surface concentration. Thus, augmentation of ξ_2 promotes the reduction of the concentration gradient that reduces the Sherwood number.

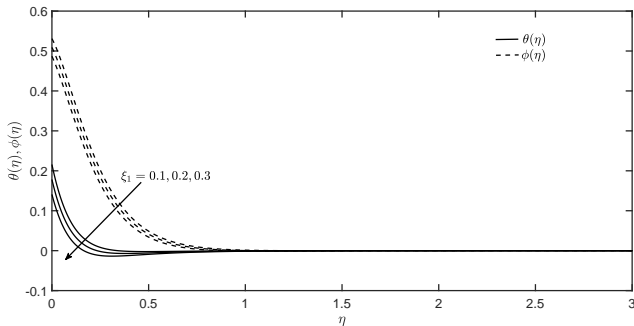


Fig. 6. Temperature and concentration profiles with varying values of thermal stratification parameter, ξ_1 .

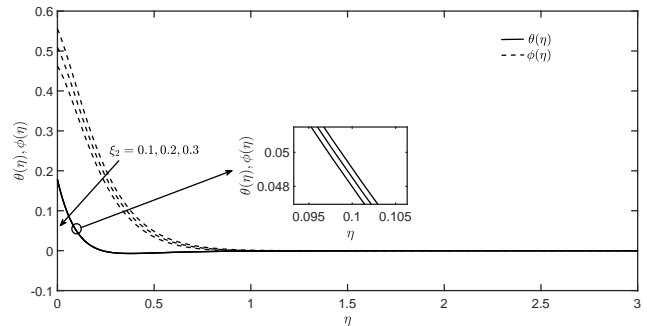


Fig. 7. Temperature and concentration profiles with varying values of solutal stratification parameter, ξ_2 .

Meanwhile, the Brownian motion in the hybrid nanofluid flow enhances the fluid temperature but reduces the concentration, as observed in Figs.8a and 8b, respectively. The random movement of nanoparticles in the base fluid stimulates collisions between them, which generate kinetic energy that can be converted into heat energy. Hence, the increase in Nb raises the temperature profile of the hybrid nanofluid and reduces the Nusselt number, as obtained in Table 2. However, the increment of Nb helps in improving the mass transfer performance of the hybrid nanofluid, as depicted by the increase in Sherwood number in Table 2.

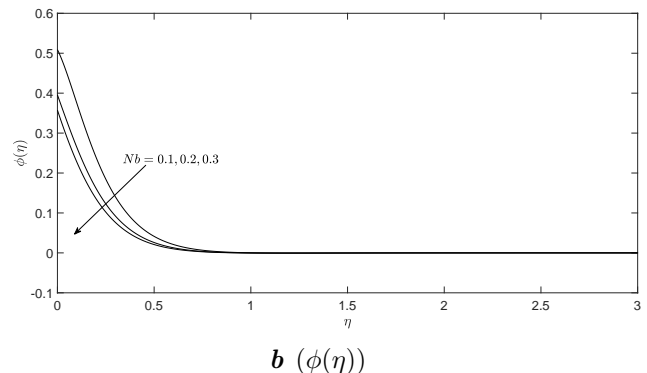
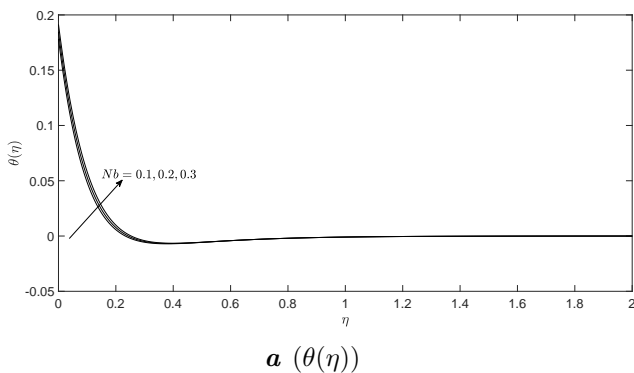


Fig. 8. Temperature and concentration profiles with varying values of Brownian motion parameter, Nb .

The incorporation of thermophoresis in the hybrid nanofluid flow increases the temperature and concentration profiles of the hybrid nanofluid, as presented in Fig. 9. The movement of hot nanoparticles near the hot sheet to the surrounding cold hybrid nanofluid enhances the temperature and concentration of the fluid. Thus, reducing the temperature and concentration gradients then lowers the rates of heat and mass transfers, as shown in Table 2.

The effects of Darcy number, Da on the velocity, temperature and concentration profiles are displayed in Fig.10. Darcy number is a parameter related to the permeability of the porous medium. The increase in Da causes the reduction of the velocity, temperature and concentration profiles of the hybrid nanofluid. However, it is observed in Fig.10 that the temperature profile increases after some distance away from the sheet. The momentum, thermal and concentration boundary layers become thinner as Da increases.

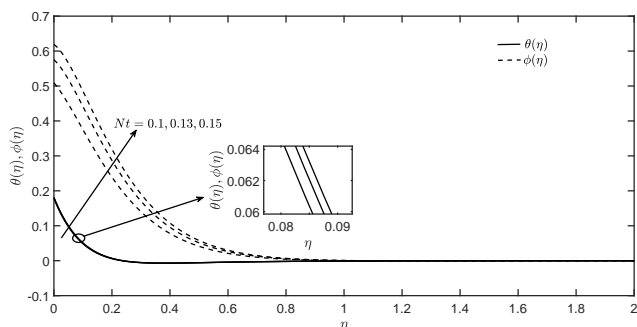


Fig. 9. Temperature and concentration profiles with varying values of thermophoresis parameter, Nt .

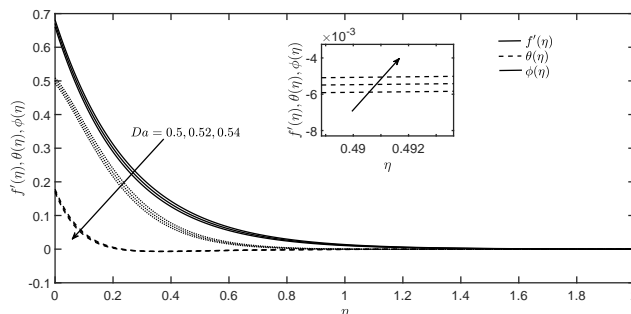


Fig. 10. Velocity, temperature and concentration profiles with varying values of Darcy number, Da .

5. Conclusion

The MHD flow of Ag-CuO/H₂O hybrid nanofluid over a permeable stretching sheet embedded in a porous medium with other effects of slips and stratification are analyzed and discussed. The Buongiorno and the Tiwari and Das nanofluid models are incorporated into the governing partial differential equations and boundary conditions. Then, these equations are simplified into a system of ordinary differential equations using appropriate similarity variables and solved numerically using the bvp4c solver. The increase in hydrodynamic slip parameter reduces the velocity profile of the hybrid nanofluid. Meanwhile, the temperature and concentration profiles diminished with the rise in thermal slip and stratification parameters. Besides that, the concentration profile is reduced by the augmentation of solutal slip and stratification parameters.

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Магнітногідродинамічний потік гібридного нанofлюїду на листі, що розтягується: ефект подвійної стратифікації та багаторазового ковзання

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Дослідження гібридних нанofлюїдів, що протікають через різні фізичні геометрії та за різних умов, є популярними серед дослідників, які хочуть зрозуміти поведінку цих рідин. У цьому дослідженні аналізуються чисельні розв'язки для потоку гібридної нанорідини Ag-CuO/H₂O по листі, який розтягується, із ефектом всмоктування, магнітним полем, подвійною стратифікацією та багаторазовим ковзанням. Для опису задачі потоку вводяться основні рівняння та крайові умови. Потім застосовуються змінні подібності з метою перетворення рівнянь у нелінійні звичайні диференціальні рівняння та крайові умови. Чисельне обчислення задачі виконано в Matlab (вирішувач bvp4c), а результати подані в таблицях і графіках. Встановлено, що збільшення параметрів ковзання та стратифікації розчинів зменшує число Шервуда. Водночас збільшення параметрів теплового ковзання та стратифікації знижує число Нуссельта. Зі збільшенням параметра гідродинамічного ковзання спостерігається збільшення коефіцієнта поверхневого тертя.

Ключові слова: гібридний нанofлюїд, подвійна стратифікація, ковзання, МГД, лист, що розтягується.